

## RESULTS FROM LAST WEEK

DENSITY-OF-STATES:  $D(\omega) = \frac{V}{2\pi^2} \frac{k^2}{\frac{d\omega}{dk}} \quad (3D)$

$$\Downarrow$$

$$D(\omega) d\omega = \frac{V}{2\pi^2} k^2 dk = \frac{V}{(2\pi)^3} 4\pi k^2 dk$$

SUM  $\rightarrow$  INTEGRAL RULE:  $\sum_{\mathbf{k}} = \left(\frac{V}{2\pi}\right)^3 \int d\bar{k} \quad (3D)$

$$= \frac{V}{(2\pi)^3} \int 4\pi k^2 dk$$

$$= \int D(\omega) d\omega$$

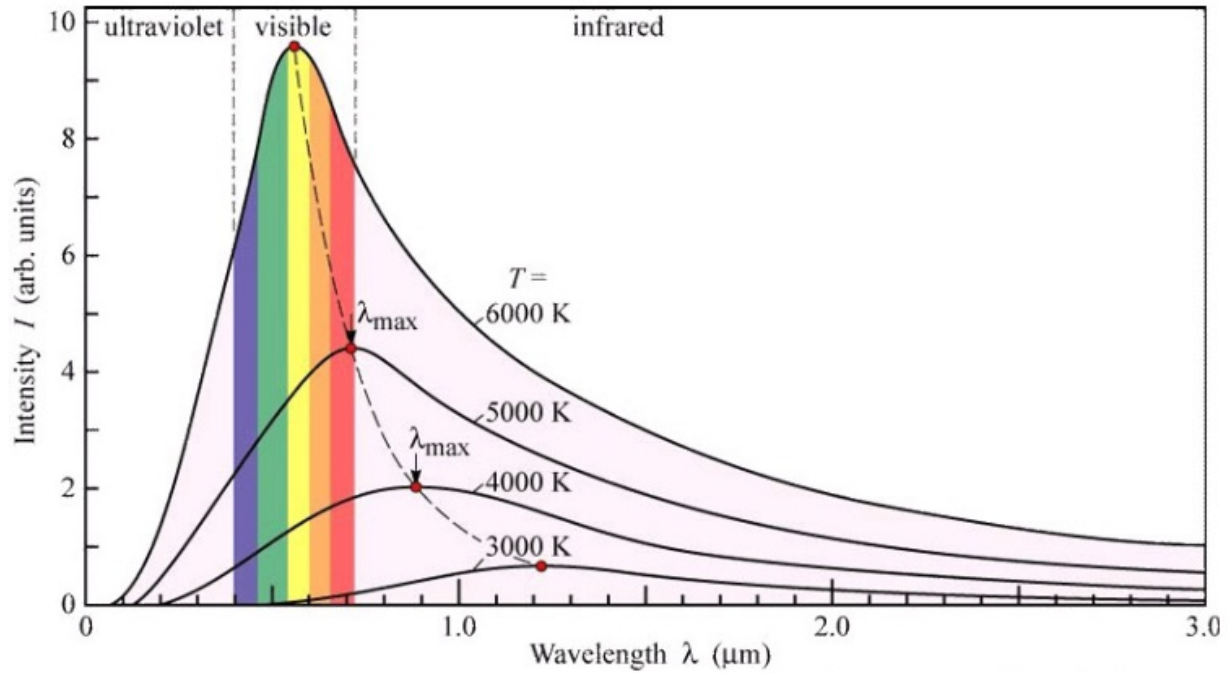
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Plank's Distribution:

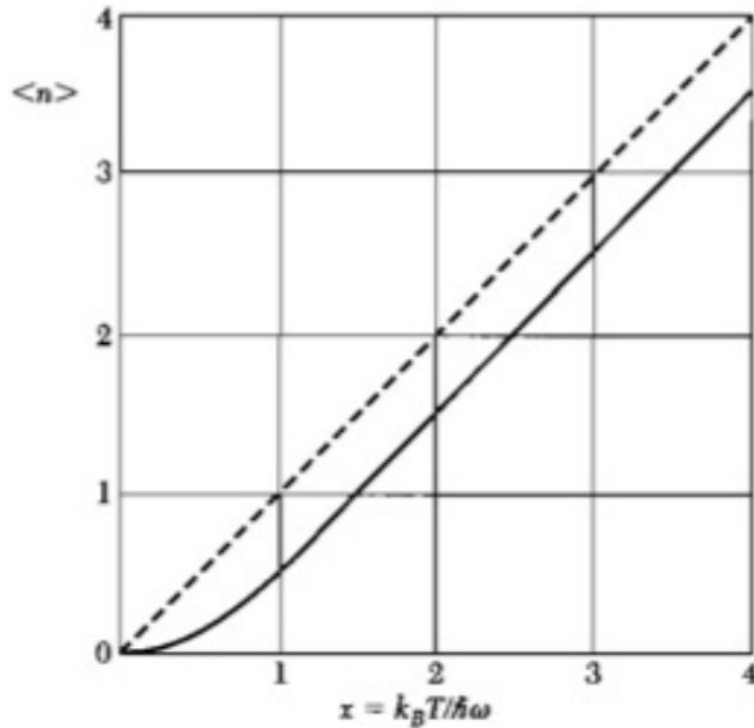
$$P(k_B T, \hbar \omega) = \frac{1}{\exp\left(\frac{\hbar \omega}{k_B T}\right) - 1}$$



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## Planck's Distribution:

$$P(k_B T, \hbar \omega) = \frac{1}{\exp\left(\frac{\hbar \omega}{k_B T}\right) - 1} = \frac{1}{\exp\left(\frac{1}{x}\right) - 1} = P(x)$$



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## SPECIFIC HEAT (HEAT CAPACITY)

$$C_V = \left( \frac{\Delta U}{\Delta T} \right)_V \rightarrow \Delta T = \frac{\Delta U}{C_V}$$

↑ specific heat coefficient

T = temperature

U = Energy of system

$$C_V = C_{\text{LATTICE}} + C_{\text{ELECTRONIC}} + \dots$$

↑  
Today

↑  
Coming lectures

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## LATTICE ENERGY

$$U_{\text{LATTICE}} = \sum_{\# \text{ modes}} P(x) \cdot \hbar \omega_k = \sum_{\# \text{ BRANCHES } k} \sum P(x) \cdot \hbar \omega_k$$

$$= \sum_{\# \text{ BRANCHES}} \int D(\omega) P(\omega, T) \hbar \omega_k d\omega$$

$$\nearrow \approx 3 \int D(\omega) P(\omega, T) \hbar \omega_k d\omega$$

Assume isotropic  
system

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WE KNOW

Phonon Dispersion

$$D(\omega) = \frac{V}{2\pi^2} \frac{A^3}{\omega^2} \quad (3D)$$

## DEBYE THEORY

$$\omega_k = v \cdot k \quad \left. \begin{array}{l} \uparrow \\ \text{sound} \\ \text{velocity} \end{array} \right\} D(\omega) = \frac{V}{2\pi^2} \left( \frac{\omega}{v} \right)^2 \frac{1}{v}$$

$$= \frac{V}{2\pi^2} \frac{\omega^2}{v^3}$$

PROBLEM:  $\int_0^\infty D(\omega) d\omega \neq N$

$\uparrow$   
# modes

"SOLUTION": DEBYE FREQUENCY (cut-off)

$$N = \int_0^{\omega_D} D(\omega) d\omega = \frac{V}{2\pi^2} \frac{1}{v^3} \left[ \frac{1}{3} \omega^3 \right]_0^{\omega_D} = \frac{V}{6\pi^2} \frac{\omega_D^3}{v^3}$$

$$\omega_D^3 = 6\pi^2 v^3 \frac{N}{V}$$

DEBYE FREQ.

$$k_D = \frac{\omega_D}{v} = \left( 6\pi^2 v^2 \frac{N}{V} \right)^{1/3}$$

DEBYE MOMENTUM

$$T_D = \frac{\hbar \omega_D}{k_B} = \frac{\hbar v}{k_B} \left( 6\pi^2 \frac{N}{V} \right)^{1/3}$$

DEBYE TEMPERATURE

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# DEBYE THEORY

$$\beta \equiv \frac{\hbar\omega}{k_B T} \quad \& \quad \beta_D \equiv \frac{\hbar\omega_D}{k_B T} = \frac{T_D}{T}$$

$$U_{\text{LATTICE}}^{\text{(DEBYE)}} = 3 \cdot \int_0^{\omega_D} D(\omega) \frac{1}{\exp\left(\frac{\hbar\omega}{k_B T}\right) - 1} \hbar\omega \, d\omega$$

$$= 9Nk_B T \left(\frac{T}{T_D}\right)^3 \int_0^{\beta_D} \frac{\beta^3}{e^{\beta} - 1} \, d\beta$$

Low-Temperature limit:

$$T \rightarrow 0; \quad \beta_D \rightarrow \infty$$

$$C_V = \frac{\partial U}{\partial T} = \frac{12\pi^4}{5} N k_B \left(\frac{T}{T_D}\right)^3$$

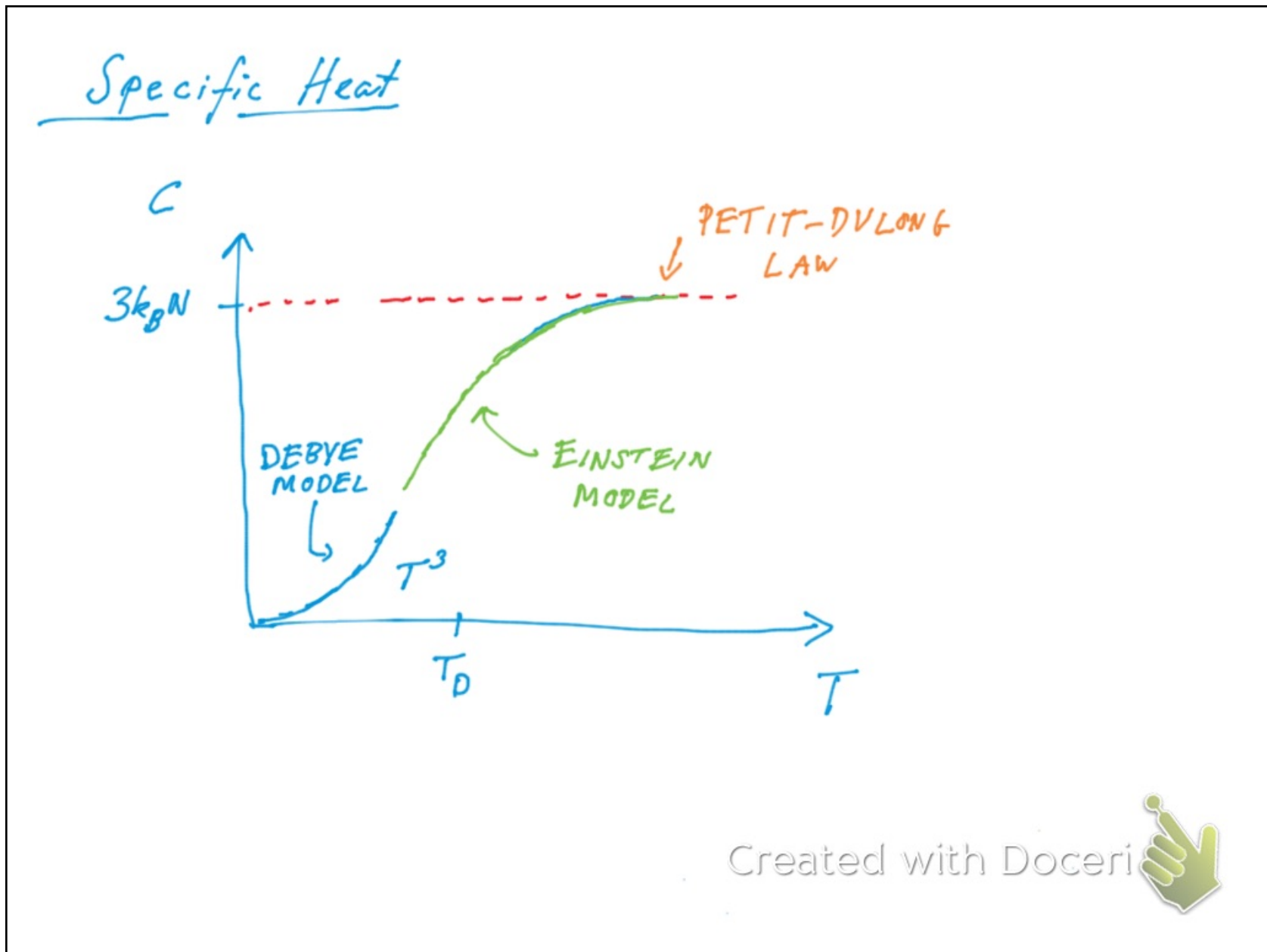
High-Temperature limit:

$$T \gg T_D; \quad \beta_D \rightarrow 0$$

$$C_V = \frac{\partial U}{\partial T} = 3Nk_B$$

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(Petit-Dulong law)





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# THERMAL CONDUCTIVITY

$P \equiv \text{Power input [WATT} = \frac{J}{s}]$   
 $A = \text{Cross-section} = t \cdot d$   
 $\kappa = \text{thermal conductivity} = \frac{P/A}{\Delta T/l} = \frac{l}{A} \cdot \frac{P}{\Delta T}$   
 $\Downarrow$   
 $\Delta T = \frac{l}{A} \frac{P}{\kappa}$

COLD END "BATH"  $T_0$   
 THERMOMETER  $T_1$   
 $\Delta T = T_2 - T_1$   
 THERMOMETER  $T_2$

HEATER / RESISTOR  
 Joules Heating

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## SPECIFIC HEAT & THERMAL CONDUCTIVITY

$$C_V = \left( \frac{\Delta U}{\Delta T} \right)_V \rightarrow \Delta T = \frac{\Delta U}{C_V}$$

↑ specific heat coefficient

T = temperature

U = Energy of system

$$C_V = C_{\text{LATTICE}} + C_{\text{ELECTRONIC}} + \dots$$

$$\kappa = \kappa_{\text{LATTICE}} + \kappa_{\text{ELECTRONIC}}$$

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